

The Monod-Wyman-Changeux model for equilibrium and kinetic O₂ binding.

To fit the kinetic parameters the Monod-Wyman-Changeux (MWC) equation was extended to incorporate rate parameters.

The MWC model, originally developed by Niesel, assumes two conformational states of the hemoglobin, T (tense) and R (relaxed). Hemoglobin may exist in ten forms, T₀₋₄ and R₀₋₄, the subscript (0-4) denoting the number of oxygen molecules bound. In each state, the four oxygen binding sites have the same oxygen affinity with oxygen binding parameters defined as K_T and K_R respectively, and rate parameters denoted k_T, k'_T, k_R and k'_R respectively, where the k is dissociation and the k' association; K=k'/k. The association can be expressed in sec⁻¹mol⁻¹ or in sec⁻¹kPa⁻¹. Since saturation is against oxygen pressure P, we will use the second form.

Since the Hb has four binding locations, from the forms T_n, R_n n molecules can dissociate so the k has to be multiplied by n, whereas 4-n molecules can associate and the k' has to be multiplied by (4-n):

$$n k_X X_n = (4-[n-1]) k'_X P X_{n-1} \quad X = R \text{ or } T, \quad n = 1-4$$

from which can be solved:

$$X_n = \binom{4}{n} (K_X P)^n X_0 = \binom{4}{n} (K_X P)^{n-4} X_4 \quad X = R \text{ or } T, \quad n = 0-4^{(1\dagger)}$$

Then, the total amount of species X, X_t, is - note, that X₄ = (K_XP)⁴X₀:

$$X_t = \sum_{n=0}^4 \binom{4}{n} (K_X P)^n X_0 = (1 + K_X P)^4 X_0 = \{1 + 1/(K_X P)\}^4 X_4 \quad X = R \text{ or } T$$

and the total amount of oxygen bound to form X, denoted here as XO₂:

$$XO_2 = \sum_{n=0}^4 n \binom{4}{n} (K_X P)^n X_0 = 4 K_X P (1 + K_X P)^3 X_0 = 4 \{1 + 1/(K_X P)\}^3 X_4 \quad X = R \text{ or } T$$

Also, a parameter is needed for the equilibrium between T and R state. Either

$$T_0 = L_0 R_0 \quad \text{or} \quad T_4 = L_4 R_4 \quad - \text{note, that } L_4 = (K_T/K_R)^4 L_0.$$

Then the total amount of hemoglobin is:

$$c_{Hb,t} = \{L_0(1 + K_T P)^4 + (1 + K_R P)^4\} R_0 = [L_4 \{1 + 1/(K_T P)\}^4 + \{1 + 1/(K_R P)\}^4] R_4$$

and the total amount of bound oxygen - note, that this can be up to 4 times the total amount of Hb:

$$c_{O_2Hb} = 4 \{L_0 K_T P (1 + K_T P)^3 + K_R P (1 + K_R P)^3\} R_0 = 4 [L_4 \{1 + 1/(K_T P)\}^3 + \{1 + 1/(K_R P)\}^3] R_4$$

so that saturation S is:

$$S = \frac{L_0 K_T P (1 + K_T P)^3 + K_R P (1 + K_R P)^3}{L_0 (1 + K_T P)^4 + (1 + K_R P)^4} = \frac{L_4 \{1 + 1/(K_T P)\}^3 + \{1 + 1/(K_R P)\}^3}{L_4 \{1 + 1/(K_T P)\}^4 + \{1 + 1/(K_R P)\}^4}$$

and the desaturation 1-S:

$$1-S = \frac{L_0 (1 + K_T P)^4 + (1 + K_R P)^4}{L_0 (1 + K_T P)^4 + (1 + K_R P)^4} = \frac{L_4 / (K_T P) \{1 + 1/(K_T P)\}^3 + 1 / (K_R P) \{1 + 1/(K_R P)\}^3}{L_4 \{1 + 1/(K_T P)\}^4 + \{1 + 1/(K_R P)\}^4}$$

^(†) $\binom{4}{n} = \frac{4!}{n!(4-n)!} = 1, 4, 6, 4, 1$ for n = 0 - 4

The definition with L_4 is useful as it was shown that the model can be fitted at a wide range of conditions by using essentially only one variable, K_T , while K_R is constant and L_4 is almost constant. Note, that the amount of 'reduced Hb' available for O_2 $c_{RedHb} = 4c_{Hb} - c_{O_2Hb}$ is:

$$c_{RedHb} = \{4L_0(1 + K_T P)^3 + (1 + K_R P)^3\} R_0 = 4[L_4/(K_T P)\{1 + 1/(K_T P)\}^3 + (1/K_R P)\{1 + 1/(K_R P)\}^3] R_4$$

The rate parameters in the MWC model are derived similarly. Dissociation k will be from the occupied sites:

$$\begin{aligned} k_{CO_2Hb} &= k_T T O_2 + k_R R O_2 = k_T 4K_T P (1 + K_T P)^3 T_0 + k_R 4K_R P (1 + K_R P)^3 R_0 \\ &= 4\{L_0 k_T K_T P (1 + K_T P)^3 + k_R K_R P (1 + K_R P)^3\} R_0 \\ \text{or} &= 4[L_4 k_T \{1 + 1/(K_T P)\}^3 + k_R \{1 + 1/(K_R P)\}^3] R_4 \end{aligned}$$

so that – note, that $k_X K_X = k'_X$:

$$k = \frac{L_0 k'_T (1 + K_T P)^3 + k'_R (1 + K_R P)^3}{L_0 K_T (1 + K_T P)^3 + K_R (1 + K_R P)^3} = \frac{L_4 k_T \{1 + 1/(K_T P)\}^3 + k_R \{1 + 1/(K_R P)\}^3}{L_4 \{1 + 1/(K_T P)\}^3 + \{1 + 1/(K_R P)\}^3}$$

And association will be to the unoccupied sites:

$$\begin{aligned} k'_{c_{RedHb}} &= k'_T (4T_t - T O_2) + k'_R (4R_t - R O_2) = k'_T 4 (1 + K_T P)^3 T_0 + k'_R 4 (1 + K_R P)^3 R_0 \\ &= 4\{L_0 k'_T (1 + K_T P)^3 + k'_R (1 + K_R P)^3\} R_0 \\ \text{or} &= 4[L_4 k'_T / (K_T P) \{1 + 1/(K_T P)\}^3 + k'_R / (K_R P) \{1 + 1/(K_R P)\}^3] R_4 \end{aligned}$$

so that – again using $k_X = k'_X / K_X$:

$$k' = \frac{L_0 k'_T (1 + K_T P)^3 + k'_R (1 + K_R P)^3}{L_0 (1 + K_T P)^3 + (1 + K_R P)^3} = \frac{L_4 k_T \{1 + 1/(K_T P)\}^3 + k_R \{1 + 1/(K_R P)\}^3}{(L_4 / K_T) \{1 + 1/(K_T P)\}^3 + (1 / K_R) \{1 + 1/(K_R P)\}^3}$$

leading to an 'apparent equilibrium parameter' – which of course is not constant:

$$K = k'/k = \frac{L_0 K_T (1 + K_T P)^3 + K_R (1 + K_R P)^3}{L_0 (1 + K_T P)^3 + (1 + K_R P)^3} = \frac{L_4 \{1 + 1/(K_T P)\}^3 + \{1 + 1/(K_R P)\}^3}{(L_4 / K_T) \{1 + 1/(K_T P)\}^3 + (1 / K_R) \{1 + 1/(K_R P)\}^3}$$

so that $KP(1-S) = S$ is indeed valid. Note, that the 'apparent P_{50} ' = $1/K$.

References:

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